# Coupled flow and geomechanics of petroleum reservoirs, aquifers and faults

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## **Computational modeling of flow, transport** and deformation

People

- Induced earthquildent
- Leakage along fa
- Hydraulic fractur
- Geothermal ene
- Underground ga
- Enhanced hydro injection



Manjunath GL

Multiscale mechanical behavior of materials ranging from engineering materials to geomaterials. MS and PhD from Indian Institute of Technology Madras, India.

M.S. Students 

#### **Injection-Induced Earthquakes**

William L. Ellsworth

Science JULY 2013



#### Natural or induced?

#### NEWS OF THE WEEK

16 JANUARY 2009 VOL 323 SCIENCE www.sciencemag.org SEISMOLOGY A Human Trigger for the Great Quake of Sichuan?

Natural disasters are often described as "acts of God," but within days of last May's devastating earthquake in China's Sichuan Province, seismologists in and out of China were quietly wondering whether humans might have had a hand in it. Now, the first researchers have gone



#### EARTHQUAKES

#### Human-induced shaking

In 2011, a modest earthquake in southern Spain seriously damaged the city of Lorca. deformation suggests that the quake was caused by rupture of a shallow fault patch pumping of water from a nearby aquifer.

#### Jean-Philippe Avouac



#### Induced earthquakes mechanisms



Healy et al., *Science* 1968 Segall, *JGR* 1985 Chander and Kalpana, *EG* 1997

### Multiphase fluid flow and geomechanics

Biot, *JAP* 1941 Rice et al, *RGSP* 1976 Coussy, 1995





Oil, water, gas have different pressures and densities.

#### Governing equations

Force balance (quasi-static):

$$\nabla \cdot \boldsymbol{\sigma} + \rho_b \boldsymbol{g} = 0$$
  $\rho_b = (1 - \phi)\rho_s + \phi \sum_{\alpha} \rho_{\alpha}$ 

Fluid mass balance:

$$\frac{\partial}{\partial t} \left( \rho_{\alpha} \sum_{\beta} \left( N_{\alpha\beta} + \frac{b_{\alpha} b_{\beta}}{K_{dr}} \right) p_{\beta} \right) + \frac{1}{K_{dr}} \frac{\partial}{\partial t} \left( \rho_{\alpha} b_{\alpha} \sigma_{v} \right) + \nabla \cdot \boldsymbol{w}_{\alpha} = \rho_{\alpha} f_{\alpha},$$

 $\alpha,\beta~$  = Oil, water, gas

#### Multiphase fluid flow and geomechanics



Coupling between flow and deformation through parameters (poroelastic properties) and processes (PDE terms)

#### Geomechanics of a fault



Effective normal stress: 
$$\sigma'_n = \sigma_n - bp$$

Friction stress:  $au_f = \mu_f \sigma'_n$ 

Mohr-Coulomb theory

Shear failure criterion:  $\tau \geq \tau_f$ 

**Coulomb Failure Function:** 

$$CFF = \tau - \mu_f \sigma'_n$$



#### Induced seismicity mechanisms



Tendency to slip if:

$$\Delta \mathrm{CFF} = \Delta \tau - \Delta \left[ \mu_f (\sigma_n - bp) \right] > 0$$

 $\begin{array}{ll} \Delta \tau > 0 & (\text{poroelastic loading}) \\ \Delta \sigma_n < 0 & (\text{poroelastic unloading}) \\ \Delta p > 0 & (\text{fluid injection}) \\ \Delta \mu_f < 0 & (\text{fault weakening}) \end{array}$ 

#### Water extraction from unconfined aquifer



$$\Delta \text{CFF} = \Delta \tau - \Delta \left[ \mu_f (\sigma_n - bp) \right] > 0$$

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#### Hydrocarbon production from confined reservoir



$$\Delta \text{CFF} = \Delta \tau - \Delta \left[ \mu_f (\sigma_n - bp) \right] > 0$$

 $\begin{array}{ll} \Delta \tau > 0 & (\text{poroelastic loading}) \\ \hline \Delta \sigma_n < 0 & (\text{poroelastic unloading}) \\ \Delta p > 0 & (\text{fluid injection}) \\ \Delta \mu_f < 0 & (\text{fault weakening}) \end{array}$ 

#### Fluid injection into a confined reservoir



$$\Delta \text{CFF} = \Delta \tau - \Delta \left[ \mu_f (\sigma_n - bp) \right] > 0$$

 $\begin{array}{ll} \Delta \tau > 0 & (\text{poroelastic loading}) \\ \Delta \sigma_n < 0 & (\text{poroelastic unloading}) \\ \hline \Delta p > 0 & (\text{fluid injection}) \\ \Delta \mu_f < 0 & (\text{fault weakening}) \end{array}$ 

#### Fault slip can lead to leakage



Fluid leakage if:  $\Delta k_f > 0$ 

 $\begin{array}{l} \Delta k_{f} = f \text{(fault slip, fault compression)} \\ \Delta \tau > 0 \quad (\text{poroelastic loading}) \\ \Delta \sigma_{n} < 0 \quad (\text{poroelastic unloading}) \\ \Delta p > 0 \quad (\text{fluid injection}) \\ \hline \Delta \mu_{f} < 0 \quad (\text{fault weakening}) \end{array}$ 

## Key questions in subsurface energy production

- How much can be extracted/stored, and at what rate?
- What is the risk of induced seismicity? What is the risk of leakage?
- How do we mitigate the risk?

Geomechanical modeling of reservoirs with faults is essential.

Settari and Mourits, *SPEJ* 1998; Bourne et al., *J Struct Geol* 2001 Birkholzer and Zhou, *IJGGC* 2009; Morris et al., *IJGGC* 2011; Cappa and Rutqvist, *GRL* 2011; Jha and Juanes, *WRR* 2014

## Computational model

#### Discretization

- Stable, convergent scheme (FEM-FVM)
- Single, unstructured computational grid

Pressure node

Displacement node

#### Jha and Juanes, *Acta Geotech.* 2007 Kim, Tchelepi and Juanes, *CMAME* 2011 Jha and Juanes, *WRR* 2014



#### Coupling strategies

Efficient, unconditionally stable sequential solution scheme

New time step  
Sequential  
iteration  
Flow  
Flow  
Fix 
$$\frac{\partial \sigma_v}{\partial t}$$
  
 $\left(\frac{b^2}{K_{dr}} + \frac{1}{M}\right)\frac{\partial p}{\partial t} + \frac{b}{K_{dr}}\frac{\partial \sigma_v}{\partial t} + \nabla \cdot \boldsymbol{v} = f$   
Nechanics known  
Mechanics  $p_g, S_w$   
Yes  
Converged?  
No

#### Aagaard, Knepley and Williams, JGR 2013

## Computational model

Fault is discretized with interface finite elements.



• Lagrange multiplier approach to solve the contact problem

$$\begin{bmatrix} \mathbf{K} & \mathbf{C}^{\mathsf{T}} \\ \mathbf{C} & \mathbf{0} \end{bmatrix}^{(k)} \begin{bmatrix} \delta \mathbf{U} \\ \delta \mathbf{L} \end{bmatrix}^{(k)} = - \begin{bmatrix} \mathbf{R}_{u} \\ \mathbf{R}_{l} \end{bmatrix}^{(k)}$$

*U* is displacement.*L* is Lagrange multiplier (fault traction)

Aagaard, Knepley and Williams, *JGR* 2013 Jha and Juanes, *WRR* 2014

## Coupled multiphase flow and geomechanics simulator



- Computationally efficient sequential solution
- Sophisticated formulation for fault deformation and slip
- Flow along and across fault, fracture propagation
- Viscoelastic, elastoplastic, and viscoplastic rheology. Rate and State fault friction
- Field-scale (unstructured grid, complex production-injection scenarios, parallel computing)

#### Post mortem analysis of the 2011 Lorca earthquake

LETTERS

## The 2011 Lorca earthquake slip distribution controlled by groundwater crustal unloading

Pablo J. González<sup>1</sup>\*, Kristy F. Tiampo<sup>1</sup>, Mimmo Palano<sup>2</sup>, Flavio Cannavó<sup>2</sup> and José Fernández<sup>3</sup>

Earthquake initiation, propagation and arrest are influenced by fault frictional properties<sup>1,2</sup> and preseismic stress<sup>3,4</sup>. Studies of triggered and induced seismicity<sup>5-7</sup> can provide unique

nature

geoscience

Methods). Two different ENVISAT descending satellite tracks (12 and 16) imaged the area before and after the event, providing estimates of the displacement field from two different look angles

PUBLISHED ONLINE: 21 OCTOBER 2012 | DOI: 10.1038/NGE01610





- 1960-2010 groundwater extraction
- Mw = 5.1 in May 2011

#### Effect of water withdrawal - Conceptual model



Drop in water table in aquifer:  $\Delta z$ 

Unloading of basement:

$$\Delta \boldsymbol{\sigma} = \boldsymbol{f}(\phi \rho_w \Delta z A, \dots)$$

Drop in pressure in basement:  $\Delta p = \Delta p_c + \Delta p_d$ (Pore expansion + pressure diffusion)

#### **Previous interpretation**

(Gonzalez et al., *Nature Geosci.* 2012 de Michele et al., *Seism. Res. Lett.* 2013)

- Ignored coupling between flow and deformation
- Ambiguous regarding which fault sourced the earthquake



Can we ignore flow-deformation coupling?

Which fault ruptured and how?

#### **Computational model**



Jha et al, AGU 2013

#### Drop in pressure and water table



#### Subsidence due to groundwater withdrawal



Jha et al, AGU 2013

#### Decrease in water table and ground subsidence



Water table data is from a few wells.

#### Change in fault stability due to water extraction



Tendency to slip if:  $\Delta CFF = \Delta \tau - \Delta [\mu_f(\sigma_n - bp)] > 0$ 

AMF fault is actually stabilized.



#### The 2012 Emilia-Romagna earthquakes

• Sequence of earthquakes ( $M_w$ = 6,  $M_w$ = 5.8) in May 2012 near the Cavone oil field in Italy



- Raised the question: *Was it induced by production/injection?*
- We address this question by means of computational modeling of coupled flow and geomechanics, integrating geologic constraints, seismic observations, and historical production

#### Effect of production - Conceptual model



Tendency to slip if:

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#### The Cavone oilfield

Map view



- Reservoir is compartmentalized by several faults.
- Strong aquifer support from underneath the reservoir.
- Oil production started in 1980. Injection of produced/ waste water began in 1993. 16 producers, 1 injector.

#### **Regional seismicity**



#### Seismicity on regional faults



Seismicity data from Jan 2011 – Feb 2013

#### **Computational model**

Structural model



#### Reservoir surfaces

#### Fault

#### Geomechanical grid



Jha et al, *AGU* 2014

# Reservoir pressure changes due to production and injection



#### Shear and normal fault tractions change due to prod/inj

![](_page_32_Figure_1.jpeg)

![](_page_32_Figure_2.jpeg)

#### Evolution of pressure and stress on fault

![](_page_33_Figure_1.jpeg)

- Increase in Coulomb stress not enough to trigger seismicity
- Injection stabilized the fault.

## Seismicity induced by CO<sub>2</sub> injection

Can CO<sub>2</sub> injection induce seismicity? Largest magnitude?

![](_page_34_Figure_2.jpeg)

![](_page_34_Figure_3.jpeg)

#### **Computational model**

![](_page_35_Figure_2.jpeg)

#### Over-pressurization due to injection

![](_page_36_Figure_1.jpeg)

# Pressure rises in the fault block where the injector is located.

 $CO_2$  accumulates near the top because of buoyancy.

#### Over-pressurization due to injection

![](_page_37_Figure_1.jpeg)

#### Fault pressure

![](_page_38_Figure_1.jpeg)

Pressure on the fault also increases in the reservoir depth interval.

![](_page_38_Figure_3.jpeg)

#### Fault slips due to over-pressurization

![](_page_39_Figure_1.jpeg)

![](_page_39_Figure_2.jpeg)

#### Fault slips due to over-pressurization

![](_page_40_Figure_1.jpeg)

# Slip area gives magnitude of seismicity

![](_page_40_Figure_3.jpeg)

Slip direction gives directivity of seismic energy released

#### Depth profiles of pressure and stresses along the fault

![](_page_41_Figure_1.jpeg)

Stress paths of specific points on the fault

![](_page_42_Figure_1.jpeg)

![](_page_42_Picture_2.jpeg)

## Influence of meteorological cycle in midcrustal seismicity of the Nepal Himalaya

Kundu et al., JAES 2017

![](_page_43_Figure_2.jpeg)

#### Evaporation induced unloading and snowfallinduced loading of the MHT fault

![](_page_44_Figure_1.jpeg)

Kundu et al., JAES 2017; Bettinelli et al., *EPSL*, 2008 Time lag between monsoon rainfall (summer) and mid-crustal seismicity (winter)

![](_page_45_Figure_1.jpeg)

Pressure change = change due to diffusion + change due to poroelastic deformation

## Coupled flow and geomechanical model

![](_page_46_Picture_1.jpeg)

Three sections of MHT

## Flat section Ramp section Aseismic section

Rainfall load from Equivalent Water Height

#### Induced changes in fault tractions

![](_page_46_Figure_6.jpeg)

![](_page_46_Figure_7.jpeg)

## Conclusions

Computational modeling of coupled flow and geomechanics is a powerful tool:

- Provides mechanistic explanation of seismicity, fluid flow, and ground deformation observed around reservoirs
- Identifies energy and groundwater extraction strategies that can mitigate seismic risk

#### **Underground gas storage**

![](_page_48_Figure_1.jpeg)

Side view

Store in summer, produce in winter. How much can be stored and how fast?

#### Finite element modeling and simulation

![](_page_49_Picture_1.jpeg)

![](_page_49_Picture_2.jpeg)

Top view

#### Compare model results with satellite data

![](_page_50_Picture_1.jpeg)